

UNCLASSIFIED

AD 4 3 7 1 9 0

DEFENSE DOCUMENTATION CENTER

FOR

SCIENTIFIC AND TECHNICAL INFORMATION

CAMERON STATION, ALEXANDRIA, VIRGINIA



UNCLASSIFIED

NOTICE: When government or other drawings, specifications or other data are used for any purpose other than in connection with a definitely related government procurement operation, the U. S. Government thereby incurs no responsibility, nor any obligation whatsoever; and the fact that the Government may have formulated, furnished, or in any way supplied the said drawings, specifications, or other data is not to be regarded by implication or otherwise as in any manner licensing the holder or any other person or corporation, or conveying any rights or permission to manufacture, use or sell any patented invention that may in any way be related thereto.

190

437190

Technical Report 17

PRELIMINARY RESULTS ON FAST LUMINOUS FRONTS IN ELECTROMAGNETIC SHOCK TUBES

By: R. A. Nelson

Prepared for:

DIRECTOR
OFFICE OF SECRETARY OF DEFENSE
ADVANCED RESEARCH PROJECTS AGENCY
WASHINGTON, D.C.

CONTRACT SD-103 UNDER
ARPA ORDER 281-62
PROJECT CODE 7400

AS

STANFORD RESEARCH INSTITUTE

MENLO PARK, CALIFORNIA

SRI



7-60

Requests for additional copies by Agencies of the Department of Defense, their contractors, and other Government agencies should be directed to the:

DEFENSE DOCUMENTATION CENTER (DDC)
CAMERON STATION
ALEXANDRIA, VIRGINIA

Department of Defense contractors must be established for DDC services or have their "need-to-know" certified by the cognizant military agency of their project or contract.

All other persons and organizations should apply to the:

U.S. DEPARTMENT OF COMMERCE
OFFICE OF TECHNICAL SERVICES
WASHINGTON 25, D.C.

STANFORD RESEARCH INSTITUTE

MENLO PARK, CALIFORNIA



November 1963

Technical Report 17

PRELIMINARY RESULTS ON FAST LUMINOUS FRONTS IN ELECTROMAGNETIC SHOCK TUBES

Prepared for:

DIRECTOR
OFFICE OF SECRETARY OF DEFENSE
ADVANCED RESEARCH PROJECTS AGENCY
WASHINGTON, D.C.

CONTRACT SD-103 UNDER
ARPA ORDER 281-62
PROJECT CODE 7400

*By: R. A. Nelson
Mathematical Physics Department*

SRI Project No. 3857

Copy No.....19

ABSTRACT

Preliminary results of a theoretical study of precursor effects in electromagnetic shock tubes are presented. In particular, an examination is made of the theories of fast luminous fronts which are observed to precede shock waves in such shock tubes. Errors in a theory by Paxton and Fowler are indicated.

CONTENTS

ABSTRACT	ii
I INTRODUCTION.	1
II CRITICISM OF PAXTON-FOWLER THEORY	3
III FIRST ORDER IONIZATION FRONT THEORY	5
IV CONCLUDING REMARKS.	9

I INTRODUCTION

This technical report contains some preliminary results of a theoretical study of precursor effects in electromagnetic shock tubes. The study was initiated to supplement the experiment work on electromagnetic shock tubes that is being conducted in the Electromagnetic Sciences Laboratory here at SRI.

Precursor ionization ahead of the first shock in electromagnetic shock tubes has been widely observed. A much less widely observed phenomenon is that of a fast luminous front preceding the first shock. The exact relationship between these two phenomena has yet to be established. This report deals primarily with results obtained on the fast luminous fronts, but the theory suggested for the luminous fronts also accounts for the precursor ionization that results from the driving discharge.

Fast luminous fronts have been observed to precede the first shock wave in electromagnetic shock tubes. Josephson and Hales¹ noted a faintly luminous front in deuterium that traveled at speeds between 30 and 120 cm/ μ sec at ambient pressures between 0.1 and 2.5 mm Hg. A conical shock tube was driven by a 3.2 μ f capacitor charged to 24 kv. They speculated on the possibility that the front was due to deuterons that were accelerated to kilovolt energies by instabilities occurring in discharge. Medford, Powell, and Fletcher² also observed a luminous front moving ahead of the first shock in deuterium. The speed of the first front was 5 cm/ μ sec at an ambient pressure of 4 mm Hg. Energy for their shock tube was supplied by a 10- μ f capacitor charged to 10 kv. They concluded that this front had the properties of a weak R-type ionization front.³ In the terminology of fluid dynamics, such a front is classified as a weak detonation front.⁴ Fowler and Hood⁵ observed fast luminous waves in hydrogen and argon. They reported velocities between 60 and 400 cm/ μ sec at pressures between 0.1 and 1 mm Hg using voltages from

¹ V. Josephson and R. W. Hales, Space Technology Laboratories Report STL/TR-60-0000-19313, 1960 (unpublished).

² R. D. Medford, A. L. T. Powell and W. H. W. Fletcher, Nature **196**, 32 (1962).

³ F. D. Kahn, Bull. Astro. Inst. Neth. **12**, 187 (1954).

⁴ R. Courant and K. O. Friedrichs, *Supersonic Flow and Shock Waves* (Interscience Publishers, New York, 1948).

⁵ R. G. Fowler and J. D. Hood, Jr., Phys. Rev. **128**, 991 (1962).

3 to 9 kv. A companion paper by Paxton and Fowler⁶ presents a theory for breakdown wave propagation and relates such waves with the observed fast luminous fronts.

A criticism of the treatment by Paxton and Fowler will be made in this note, and it will be hypothesized that breakdown waves can be treated as ionization fronts to first order, with electrical current constituting a second-order effect.

⁶ G. W. Paxton and R. G. Fowler, Phys. Rev. **128**, 993 (1962).

II CRITICISM OF PAXTON-FOWLER THEORY

Paxton and Fowler⁶ consider the propagation of luminosity fronts associated with the electrical breakdown of a gas. A breakdown wave front was treated as an electron shock wave. They presumed that near the electrode where the potential gradient in the gas is greatest, ionization of a small quantity of gas occurs and that the electrons produced are given kinetic energy by the electric field. The resulting localized high-temperature electron gas is considered to expand rapidly, thus producing an electron shock wave which propagates into the ambient gas, partially ionizing the overrun neutral gas molecules. An inconsistency in their paper results from the statement that "the energy necessary for driving the shock wave is given directly to the electrons in the shock zone by the external field;" actually their treatment indicates—as they later state explicitly—that there is only a secondary dependence of the propagation speed on the direct effect of the electric field. The primary driving mechanism in their treatment is the partial pressure of high-temperature electrons behind the front.

They use a one-dimensional, steady-state, three-fluid, hydro-dynamical model assuming that the electron pressure is much greater than the partial pressures of the other species, that there is no electrical current, and that there is negligible heat flow. The principal criticism of their paper lies in their treatment of the zero electrical current assumption. As a first-order condition their assumption seems quite reasonable, but they express this condition as follows:

$$nv - N_i V_i = 0 \quad (1)$$

where

n = Number density of electrons

v = Flow velocity of electrons in the frame in which the front is at rest

N_i = Number density of ions

V_i = Flow velocity of ions in the frame in which the front is at rest.

Actually this equation is the steady-state expression for charge conservation across the front (*i.e.*, ahead of the front there are no electrons or positive ions and at the front the same number of free electrons and singly ionized positive ions are generated; thus $nv = N_i V_i$ both ahead of and behind the front). The condition for zero electrical current should be written in terms of the corresponding velocities in the laboratory frame. Thus

$$n(v - V_0) - N_i(V_i - V_0) = 0 \quad (2)$$

where V_0 is the speed of the front. Except for the trivial case in which $V_0 = 0$, these two equations imply that $N_i = n$ and $V_i = v$. Hence the ions and electrons would travel together, and a three-fluid model is not necessary for a zero-current model.

As a result of the misinterpretation of Eq. (1) the solution given by Paxton and Fowler does have current flowing in the laboratory frame. And since the electron flow is in the same direction as the front velocity while the ions are virtually stationary, this gives the unlikely result that current flows against the electric field for the case of a breakdown wave originating at a positive electrode. On the other hand, a model of this kind may have merit for the case of a precursor wave traveling into an essentially field-free region.

III FIRST-ORDER IONIZATION-FRONT THEORY

An alternative method that appears promising for the treatment of both breakdown waves and precursor waves is to treat these phenomena as ionization fronts, as suggested by Medford, Powell and Fletcher.² To first order, the luminous front preceding a shock wave in an electromagnetic shock tube will be considered to be the same as a breakdown wave in a gaseous electrical discharge. It is assumed that the breakdown initiates at the electrode with the greatest potential gradient and that a localized region of hot ionized gas is formed. Ionizing radiation from this hot gas is assumed to be the primary driving mechanism for an ionization front that moves out from the hot gas. It is further assumed that to first order there is no electrical current; hence, a single-fluid model will be used.

Consider a one-dimensional picture. Monochromatic ionizing radiation is coming from the negative x -direction and is being absorbed at the ionization front. An ionization front consists of a comparatively thin photoabsorbing region situated between transparent ionized gas behind the front and opaque un-ionized gas ahead of the front. The front moves in the positive x -direction into the un-ionized gas at a velocity, V_0 , that is determined by the intensity of the ionizing radiation.

The ratio of specific heats will be taken to be $5/3$ (i.e., monatomic molecules are assumed), so the speed of sound, c_0 , in the ambient gas is $[(5 p_0)/(3 \rho_0)]^{1/2}$ where p_0 is the ambient pressure and ρ_0 is the ambient density. The one-dimensional fluid-dynamic equations for transfer of mass, momentum, and energy in the rest frame of the front are

$$\rho_1 v_1 = \rho_0 V_0 \quad (3)$$

$$p_1 + \rho_1 v_1^2 = p_0 + \rho_0 V_0^2 \quad (4)$$

$$\frac{5}{2} \frac{p_1}{\rho_1} + \frac{1}{2} v_1^2 = \frac{5}{2} \frac{p_0}{\rho_0} + \frac{1}{2} V_0^2 + \frac{1}{2} Q^2 \quad (5)$$

where $(1/2)Q^2$ is the excess kinetic energy per unit mass available after ionization of an atom, and is defined by

$$\frac{1}{2} mQ^2 = h\nu - E_i \quad (6)$$

with m = mass of an atom, h = Planck's constant, ν = frequency of the ionizing radiation, and E_i = ionization energy.

Define

$$\epsilon = \frac{\rho_1}{\rho_0} \quad . \quad (7)$$

Then by Eqs. (3), (4), and (5) the equation for ϵ is

$$\left[\frac{5p_0}{\rho_0} + V_0^2 + Q^2 \right] \epsilon^2 - 5 \left[\frac{p_0}{\rho_0} + V_0^2 \right] \epsilon + 4V_0^2 = 0 \quad (8)$$

or, in terms of the speed of sound in the ambient gas,

$$(3c_0^2 + V_0^2 + Q^2)\epsilon^2 - (3c_0^2 + 5V_0^2)\epsilon + 4V_0^2 = 0 \quad . \quad (9)$$

Kahn³ has enumerated the possible solutions of Eq. (9) and related them to different kinds of fronts. The kind of front that is applicable here is a weak *R*-type ionization front. It is characterized by a speed of propagation that is supersonic both with respect to the ambient gas ahead of the front and the ionized gas behind the front. A necessary condition thus obtained from Eq. (9) for the existence of such a front is

$$V_0 > \frac{1}{3} [2Q + (4Q^2 + 9c_0^2)^{1/2}] \quad . \quad (10)$$

In practice this condition is easily met since ionization of molecules typically requires radiation at wavelengths of many hundreds of Angstroms while for Q to be of comparable magnitude to V_0 at 10^8 cm/sec, radiation near one Angstrom would be required. Any source with most of its ionizing radiation at wavelengths greater than 1 \AA would certainly fulfill this condition. Actually one would expect that $V_0 \gg Q, c_0$ so that $\epsilon \approx 1$ and $v_1 \approx V_0$. Thus in the laboratory frame the magnitude of flow

speed of the ionized fluid would be much smaller than the rate of advance of the ionization front, so that to a good approximation the flow speed of the ionized fluid is zero.

A model of such an ionization front, for which the shape of the ionization density contour is easily calculable, is as follows: Consider a one-dimensional model in which a source of ionizing radiation with a flux J_0 photons/cm² sec is located at $x = -\infty$. Assume that only the neutral molecules are effective in the absorption of radiation, that the absorption of each photon gives rise to a single ion-electron pair and that the argument of all dependent variables is given by $\zeta = x - V_0 t$ for t finite. The equation for the absorption of the radiation flux is given by

$$\frac{\partial J(\zeta)}{\partial \zeta} = -\alpha J(\zeta) n_n(\zeta) \quad (11)$$

where α is the absorption coefficient and $n_n(\zeta)$ is the number density of neutral molecules. Using the boundary condition $J(-\infty) = J_0$ gives

$$J(\zeta) = J_0 \exp \left\{ -\alpha \int_{-\infty}^{\zeta} n_n(z) dz \right\} . \quad (12)$$

Let the ambient density of neutral molecules be $n_0 = n_n(\infty)$ and define $\zeta = 0$ by the condition $n_n(0) = (n_0/2)$. Then

$$J(\zeta) + V_0 n_n(\zeta) = J_0 \quad (13)$$

and the speed of the front is

$$V_0 = \frac{J_0}{n_0} . \quad (14)$$

From Eqs. (12), (13), and (14), the integral equation for the shape of the front is

$$n_0 = n_n(\zeta) + n_0 \exp \left\{ -\alpha \int_{-\infty}^{\zeta} n_n(z) dz \right\} \quad (15)$$

with $\alpha > 0$, one obtains

$$n_n(\zeta) = \frac{n_0}{1 + \exp(-\alpha n_0 \zeta)} \quad (16)$$

for the neutral molecules. Thus the number density of the ions and electrons is given by

$$n_i(\zeta) = n_e(\zeta) = \frac{n_0}{1 + \exp(\alpha n_0 \zeta)}$$

IV CONCLUDING REMARKS

It appears that the principal difference between a breakdown wave moving between a pair of electrodes and a fast luminous front moving away from the driving discharge in an electromagnetic shock tube may lie in the presence or absence of current flow, respectively. As a breakdown wave moves out from the initiating electrode, the electrode is in effect being extended into the gas. Thus there is a redistribution of surface charge over the advancing surface of the ionization front. This current flow is relatively small and can be considered as a second-order effect.

It has been assumed in the foregoing argument that radiation from the hot gas is the driving mechanism. Soft X-ray emission due to bombardment of the initiating electrode can also provide a contribution.

Medford, Powell, and Fletcher² calculate that an ionizing photon flux of 3.5×10^{23} photons/cm² sec is required to account for a speed of 5×10^5 cm/sec at a pressure of 4 mm Hg. It is interesting to note that this same flux would give a speed of about 1.1×10^8 cm/sec at 0.1 mm Hg, which gives order-of-magnitude agreement with the observations of Josephson and Hales,¹ as well as Fowler and Hood.⁵

DISTRIBUTION LIST

ORGANIZATION	NO. OF COPIES	ORGANIZATION	NO. OF COPIES
Director Office of Sec. of Defense Washington 25, D.C. Attn: Clifford E. McLain	6	U.S. Signal Missile Support Agency White Sands Missile Range New Mexico	1
Office of Director Defense Research and Engineering Weapons Systems Evaluation Group The Pentagon Washington 25, D.C.	1	Headquarters U.S. Army Air Defense Command Ent Air Force Base Colorado Springs, Colorado	1
Department of the Army Office, Chief of Ordnance Washington 25, D.C.	1	Bureau of Naval Weapons Navy Department Washington 25, D.C.	1
Army Missile Command Redstone Arsenal, Alabama Attn: AMSM-RMV/Re-Entry Physics Branch	1	U.S. Navy Electronics Laboratory San Diego 52, California	1
Research Laboratories General Motors Corporation Warren, Michigan Attn: Dr. Nils L. Muench	2	U.S. Naval Missile Center Advanced Programs Department Point Mugu, California	1
Army Missile Command Liaison Office Bell Telephone Laboratories Whippany, New Jersey	1	U.S. Naval Research Laboratory Washington 25, D.C.	1
U.S. Army Ordnance Diamond Ordnance Fuze Laboratories Washington 25, D.C. Attn: Dr. B. Altmann	1	U.S. Navy Headquarters Pacific Missile Range Point Mugu, California	1
Ordnance Technical Intelligence Agency Arlington Hall Station Arlington 12, Virginia	1	Headquarters North American Air Defense Command Ent Air Force Base Colorado Springs, Colorado	1
U.S. Army Ordnance Picatinny Arsenal Dover, New Jersey	1	Space Intelligence Division Headquarters, North American Air Defense Command Ent Air Force Base Colorado Springs, Colorado	1
U.S. Army, Office, Chief of Research and Development Department of the Army Washington 25, D.C.	1	Hughes Aircraft Company Florence and Temple Streets Building 5, MS B-105 Culver City, California	1
8533 DU U.S. Army Technical Branch Collection Division OACSI, DA The Pentagon, 2B457 Washington 25, D.C.	1	MIT Lincoln Laboratories Lexington, Mass. Attn: Dr. Seymour Edelberg	1
Defense Documentation Center Cameron Station Alexandria, Virginia	20	MIT Lincoln Laboratories Lexington, Mass. Attn: Aaron Galvin	1
		Syracuse University Research Corporation University Station Syracuse 10, New York	1
		Aero-Jet General Corporation Azusa, California	1
		Aerospace Corporation P.O. Box 95085 Los Angeles 45, California Attn: Library Technical Documents Group	1

DISTRIBUTION LIST *Continued*

ORGANIZATION	NO. OF COPIES	ORGANIZATION	NO. OF COPIES
Ford Motor Company Aeronutronic Division Ford Road Newport Beach, California Attn: Acquisitions Librarian	1	Martin Company Denver Division Mail #A-314 Denver 1, Colorado	1
General Dynamics Astronautics Division San Diego 12, California	1	The Mitre Corporation Middlesex Turnpike Bedford, Massachusetts	1
General Dynamics Convair Division San Diego 12, California	1	North American Aviation, Inc. General Offices 1700 East Imperial Highway El Segundo, California Attn: Dr. Charles W. Cook	1
General Dynamics Electronics Military Products Division San Diego 12, California	1	Northrop Corporation Nortronics Division Research Park	1
General Electric Company Space Sciences Laboratory Space Technology Center King of Prussia, Pennsylvania Attn: Joseph Farber	1	Palo Verdes Estates, California Attn: Kudumalakunte N. Satyendra	
General Electric Company, TEMPO 735 State Street Santa Barbara, California Attn: Walter Hausz	1	Radio Corporation of America Major Defense Systems Division Building 127-311	1
General Electric Company Heavy Military Electronics Dept. Building 9, Room 29 Court Street Plant Syracuse, New York Attn: John P. Costas	1	Moorestown, New Jersey Attn: Heinrich O. Benecke Attn: Mr. Benedict Kingsley	
General Motors Corporation Defense Systems Division Box T Santa Barbara, California Attn: Arnold T. Nordsieck	1	Radio Corporation of America Missile and Surface Radar Division Building 108-207	1
General Motors Corporation Defense Systems Division Box T Santa Barbara, California Attn: C. M. Shaar	1	Moorestown, New Jersey Attn: Archie Gold	
Geophysics Corporation of America Burlington Road Bedford, Massachusetts Attn: Jean Irl Francis King	1	Radio Corporation of America Missile and Surface Radar Division Benton Landing Road	1
Hughes Aircraft Company Fullerton, California	1	Moorestown, New Jersey Attn: Alvin David Gottlieb	
Institute for Defense Analyses 1825 Connecticut Avenue, N.W. Washington 9, D.C. Attn: John Joseph Martin	1	The RAND Corporation 1700 Main Street	1
ITT Federal Laboratories 225 Santa Monica Blvd. Santa Monica, California	1	Santa Monica, California	
Lockheed Corporation California Division Burbank, California Attn: Library	1	Baytheon Company Missile and Space Division Santa Barbara, California	1
		Baytheon Company Missile and Space Division Hartwell Road	1
		Bedford, Massachusetts	
		Space Technology Laboratories, Inc P.O. Box 95001	1
		Los Angeles 45, California	
		Sperry Rand Corporation Sperry Gyroscope Company Division	1
		Great Neck, New York	
		Westinghouse Electric Corporation Box 746	1
		Baltimore, Maryland	
		Commander U.S. Naval Weapons Laboratory Dahlgreen, Virginia	1
		Attn: Code KRT-Mode	

DISTRIBUTION LIST *Continued*

ORGANIZATION	NO. OF COPIES	ORGANIZATION	NO. OF COPIES
U.S. Air Force Aeronautical Systems Division Wright-Patterson Air Force Base, Ohio	1	Avco Corporation 201 Lowell Street Wilmington, Massachusetts	1
U.S. Air Force Aeronautical Systems Division Detachment 4 Eglin Air Force Base, Florida	1	Avco-Everett Research Laboratory 2385 Revere Beach Parkway Everett, Massachusetts	1
U.S. Air Force Ballistic Systems Division Air Force Unit Post Office Los Angeles 45, California	1	Barnes Engineering Company 30 Commerce Road Stamford, Connecticut	1
U.S. Air Force Air Force Cambridge Research Laboratories Laurence G. Hanscom Field Bedford, Massachusetts	1	Battelle Defender Battelle Memorial Institute 505 King Avenue Columbus 1, Ohio Attn: Reports Library, Room 6A	1
U.S. Air Force Air Force Cambridge Research Laboratories Laurence G. Hanscom Field Bedford, Massachusetts Attn: Norman Wolfson Rosenberg	1	Bell Telephone Laboratories, Inc. Technical Information Library Whippany Laboratory Whippany, New Jersey 07981 Attn: Technical Reports Librarian	1
National Aeronautics & Space Administration Ames Research Center Moffett Field, California	1	Bendix Corporation Bendix Systems Division 3300 Plymouth Road Ann Arbor, Michigan	1
Armour Research Foundation 10 W. 35th Street Chicago 16, Illinois	1	Bendix Corporation Bendix Radio Division Towson 4, Maryland	1
University of Chicago Laboratories for Applied Sciences Chicago 37, Illinois	1	The Boeing Company Aerospace Division Seattle 24, Washington	
Electronics Research Laboratories Columbia University New York 27, New York Attn: Lawrence H. O'Neill	1	Chance Vought Corporation Dallas 22, Texas	1
Cornell Aeronautical Laboratory, Inc. 4455 Genesee Street Buffalo 21, New York	1	Chrysler Corporation Missile Division P.O. Box 2628 Detroit 31, Michigan	1
Denver Research Institute University of Denver University Park Denver 10, Colorado	1	Defense Research Corporation 4050 State Street Santa Barbara, California Attn: Ben Alexander	1
Research Laboratory of Electronics Massachusetts Institute of Technology Cambridge 39, Massachusetts Attn: George Graham Harvey	1	Douglas Aircraft Company 3000 Ocean Park Boulevard Santa Monica, California	1
Massachusetts Institute of Technology Aerophysics Laboratory Cambridge 39, Massachusetts	1	Electro-Optical Systems, Inc. 125 North Vinedo Avenue Pasadena, California	1
Massachusetts Institute of Technology Lincoln Laboratory P.O. Box 73 Lexington 73, Massachusetts Attn: Glen F. Pippert	1	Lockheed Corporation Missile and Space Divisions Palo Alto, California Attn: Library	1
Purdue University Lafayette, Indiana Attn: Dr. Robert Goulard	1	Lockheed Corporation Missiles and Space Divisions Sunnyvale, California Attn: Library	1

DISTRIBUTION LIST Concluded

ORGANIZATION	NO. OF COPIES	ORGANIZATION	NO. OF COPIES
Sylvania Electronics Products, Inc. Electronic Defense Laboratories Mt. View, California	1		
Sylvania Electrical Products, Inc 100 - 1st Avenue Waltham 54, Massachusetts	1		
Air University Library U.S. Air Force Maxwell Air Force Base, Alabama Attn: AAL-3T-62-878a Elizabeth Perkins Document Librarian	1		
System Development Corporation 2500 Colorado Avenue Santa Monica, California	1		
Headquarters Ballistic Systems Division Air Force Systems Command Norton A.F.B., California	1		
IRIA Institute of Science and Technology The University of Michigan Box 618 Ann Arbor, Michigan Attn: William Wolfe Group Supervisor, IRIA	1		
Institute of Science & Technology The University of Michigan P.O. Box 618 Ann Arbor, Michigan Attn: BAMIRAC Library	1		
Commanding General White Sands Missile Range New Mexico Attn. Technical Library	1		
Avco Corporation 201 Lowell Street Wilmington, Massachusetts Attn: Dr. P. W. Constance	1		
Scientific and Technical Information Facility P.O. Box 5700 Bethesda, Maryland 20014 Attn: NASA Rep. (SAK/DL)	2		

**STANFORD
RESEARCH
INSTITUTE**

**MENLO PARK
CALIFORNIA**

Regional Offices and Laboratories

Southern California Laboratories
820 Mission Street
South Pasadena, California 91031

Washington Office
808-17th Street, N.W.
Washington, D.C. 20006

New York Office
270 Park Avenue, Room 1770
New York, New York 10017

Detroit Office
1025 East Maple Road
Birmingham, Michigan 48011

European Office
Pelikanstrasse 37
Zurich 1, Switzerland

Japan Office
Nomura Security Building, 6th Floor
1-1 Nihonbashidori, Chuo-ku
Tokyo, Japan

Retained Representatives

Toronto, Ontario, Canada
Cyril A. Ing
67 Yonge Street, Room 710
Toronto 1, Ontario, Canada

Milan, Italy
Lorenzo Franceschini
Via Macedonio Melloni, 49
Milan, Italy

UNCLASSIFIED

UNCLASSIFIED